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NON-HOLONOMIC SYSTEMS IN VIEW OF HAMILTONIAN PRINCIPLE

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1. INTRODUCTORY REMARKS

1.1. Physical and engineering motivation

- Dynamic systems modeling:
- classical mechanics, applications in engineering,
 - control of mobile robots, aero, naval and space vehicles,
 - modern approach of electromagnetism,
 - fluid mechanics, aeroelasticity, fluid-structure interaction,
 - dynamics of multi-phase mixtures (suspension, aerosol, magnetic fluid, etc),
 - climatology and meteorology,
 - description of relativistic particles with spin,
 - formulation of string theory,
 - chemical processes and reactors,
 - neuro-physiology and other medical disciplines,
 - biomechanics and life sciences,
 - social processes: economy, sociology, psychology, management, etc.
 - transportation, logistics.

1.2. View of classical dynamics and related disciplines

Basic principles:

- Hamiltonian principle and Lagrangian formalism,
- Appell - Gibbs function,
- d'Alembert, Jourdain, Gauss, Appell-Chetayev, etc.

Higher Dynamic Systems:

- systems with non-holonomic constraints of higher order (linear or nonlinear),
- one-sided and other non-continuous links,
- indefinite description of the system,
- higher order time derivatives in energy functional,
- requests on the system movement and trajectory character,
- trajectory planning and on-line control,
- stability testing, post-critical response nearby bifurcation points and homo-/hetero-clinic orbits.

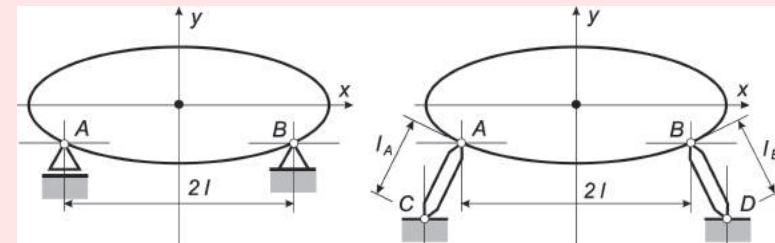
2. BASIC CONSIDERATIONS

2.1. Holonomic and non-holonomic constraints

Holonomic constraints:

linear: $\Psi(t) \cdot \mathbf{u}(t) = 0, \quad \Psi(t) \in \mathbb{R}^{l,n}, \quad \mathbf{u}(t) \in \mathbb{R}^n$

nonlinear: $\psi(\mathbf{u}, t) = 0, \quad \psi(\mathbf{u}, t) \in \mathbb{R}^l, \quad 0 \leq l \leq n,$



$$u_y(A) = 0, \quad u_x^2(A) + u_y^2(A) = l_A^2,$$

$$u_x(B) = 0, u_y(B) = 0. \quad u_x^2(B) + u_y^2(B) = l_B^2,$$

Non-holonomic constraints of the first order:

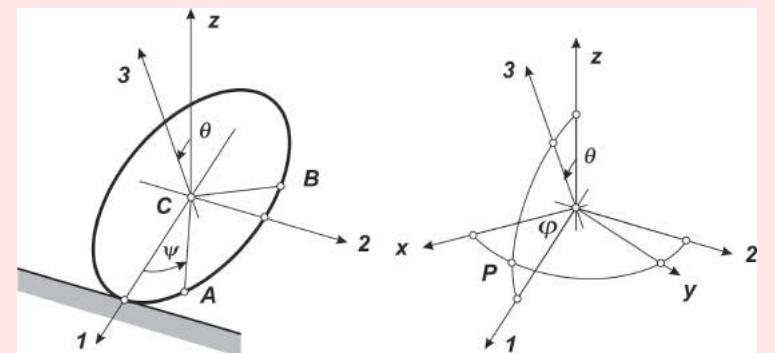
linear: $\Phi(\mathbf{u}, t) \cdot \dot{\mathbf{u}}(t) + \chi(\mathbf{u}, t) = 0, \quad \Phi(\mathbf{u}, t) \in \mathbb{R}^{l,n}, \quad \chi(\mathbf{u}, t) \in \mathbb{R}^l.$

nonlinear: $\varphi(\mathbf{u}, \dot{\mathbf{u}}, t) = 0, \quad \varphi(\mathbf{u}, t) \in \mathbb{R}^l, \quad 0 \leq l \leq n.$

n - number of degrees of freedom,

l - number of constraints,

$k = n - l$ - effective number of degrees of freedom.



Constraints differentiation → linear constraints of the 2nd order:

$\varphi^*(\mathbf{u}, \dot{\mathbf{u}}, t) \cdot \ddot{\mathbf{u}} + \dot{\varphi}(\mathbf{u}, \dot{\mathbf{u}}, t) = 0 \quad \varphi^*(\mathbf{u}, \dot{\mathbf{u}}, t) \in \mathbb{R}^{l,n} \quad 0 \leq l \leq n,$

$\varphi^*(\mathbf{u}, \dot{\mathbf{u}}, t)$ - matrix of total derivatives of the vector $\varphi(\mathbf{u}, \dot{\mathbf{u}}, t)$

$\dot{\varphi}(\mathbf{u}, \dot{\mathbf{u}}, t)$ - scalar time derivatives of the vector $\varphi(\mathbf{u}, \dot{\mathbf{u}}, t)$

Non-holonomic constraints of the $q - th$ order:

linear: $\Phi(\mathbf{u}, \dots, \mathbf{u}^{(q-1)}, t) \cdot \mathbf{u}^{(q)} + \chi(\mathbf{u}, \dots, \mathbf{u}^{(q-1)}, t) = 0, \quad (\mathbf{u}^{(1)} = \dot{\mathbf{u}})$

nonlinear: $\varphi(\mathbf{u}, \mathbf{u}^{(1)}, \dots, \mathbf{u}^{(q)}, t) = 0,$

q - highest derivative in constraints; q can be higher than the order of movement equations

$\mathbf{u}^{(1)}, \dots, \mathbf{u}^{(q)}$ - 1st,..., q -th derivative with respect to time; defined on $2n + 1$ manifold ,

Constraints differentiation → linear constraints of the $q + 1$ st order:

$\varphi^{*T}(\mathbf{u}, \mathbf{u}^{(1)}, \dots, \mathbf{u}^{(q)}, t) \cdot \mathbf{u}^{(q+1)} + \dot{\varphi}(\mathbf{u}, \mathbf{u}^{(1)}, \dots, \mathbf{u}^{(q)}, t) = 0, \quad \varphi^*(\mathbf{u}, \dot{\mathbf{u}}, t) \in \mathbb{R}^{l,n} \quad 0 \leq l \leq n$

Some domains of occurrence:

- special problems of classical mechanics,
- robotics (mobile robots),
- control of trajectories (space and naval engineering),
- neuro-physiology, life sciences
- particle physics,
- non-smooth and discontinuous constraints,
- one-sided variations,
- iso-perimetric problems, reflective extremals.
- and many others.

2.2. Definition of a holonomic and non-holonomic system

Holonomic, 1st order non-holonomic constraints - Appell & Chetayev definition:

$$\boldsymbol{\Phi}(\mathbf{u}, t)\delta\mathbf{u} = 0, \quad \text{resp.} \quad \nabla_{\mathbf{u}^{(1)}}\boldsymbol{\varphi}^T(\mathbf{u}, \mathbf{u}^{(1)}, t)\delta\mathbf{u} = 0,$$

$$\delta\mathbf{u} = [\delta u_1, \dots, \delta u_n]^T$$

- vector of virtual displacements

$$\nabla_{\mathbf{u}^{(1)}} = [\partial/\partial u_1^{(1)}, \dots, \partial/\partial u_n^{(1)}]^T$$

- 1st derivatives operator with respect to velocities $u_1^{(1)}, \dots, u_n^{(1)}$

q -th order nonholonomic constraints - Appell & Chetayev definition:

$$\boldsymbol{\Phi}(\mathbf{u}, \dots, \mathbf{u}^{(q-1)}, t)\delta\mathbf{u} = 0, \quad \text{resp.} \quad \nabla_{\mathbf{u}^{(q)}}\boldsymbol{\varphi}^T(\mathbf{u}, \dots, \mathbf{u}^{(q)}, t)\delta\mathbf{u} = 0.$$

Appell-Chetayev system; guarancy of results equivalence (d'Alembert, Jourdain, Gauss, etc.)

Hamiltonian functional:

$$\delta\mathcal{S}\{\mathbf{u}\} = \int_0^{t_1} \delta (\mathcal{T}(t) - \mathcal{V}(t)) dt = 0$$

$\mathcal{T}(t) = \mathcal{T}(\mathbf{u}, \dot{\mathbf{u}}, \dots, \mathbf{u}^{(p)}, t)$ - kinetic energy, $\mathcal{V}(t) = \mathcal{V}(\mathbf{u}, t)$, $\dot{\mathbf{u}} = \mathbf{u}^{(1)}, \dots$ - potential energy.

Assumption:

$$\mathbf{u}^*(t, \kappa) = \mathbf{u}(t) + \kappa \cdot (\tilde{\mathbf{u}}(t) - \mathbf{u}(t)) = \mathbf{u}(t) + \kappa \cdot \delta\mathbf{u}(t),$$

Approximation:

$$\delta\mathcal{S}\{\mathbf{u}\} = \lim_{\kappa \rightarrow 0} \left[\frac{d}{d\kappa} \int_0^{t_1} \left(\mathcal{T}(\mathbf{u}(t, \kappa), \mathbf{u}^{(1)}(t, \kappa), \dots, \mathbf{u}^{(p)}(t, \kappa)) - \mathcal{V}(\mathbf{u}(t, \kappa)) \right) dt \right],$$

$$\delta\mathcal{S}\{\mathbf{u}\} = \int_0^{t_1} [\nabla_{\mathbf{u}^{(p)}}^T \mathcal{T}(t) \delta\mathbf{u}^{(p)} + \dots + \nabla_{\mathbf{u}^{(1)}}^T \mathcal{T}(t) \delta\mathbf{u}^{(1)} + \nabla_{\mathbf{u}}^T (\mathcal{T}(t) \delta\mathbf{u} - \mathcal{V}(t)) \delta\mathbf{u}] dt = 0,$$

$$\delta\mathcal{S}\{\mathbf{u}\} = \int_0^{t_1} \left[(-1)^p \frac{d^p}{dt^p} (\nabla_{\mathbf{u}^{(p)}}^T \mathcal{T}(t)), \dots, -\frac{d}{dt} (\nabla_{\mathbf{u}^{(1)}}^T \mathcal{T}(t)) + \nabla_{\mathbf{u}}^T (\mathcal{T}(t) - \mathcal{V}(t)) \right] \delta\mathbf{u} dt = 0,$$

$$(-1)^p \frac{d^p}{dt^p} (\nabla_{\mathbf{u}^{(p)}}^T \mathcal{T}(t)), \dots, -\frac{d}{dt} (\nabla_{\mathbf{u}^{(1)}}^T \mathcal{T}(t)) + \nabla_{\mathbf{u}}^T (\mathcal{T}(t) - \mathcal{V}(t)) = 0.,$$

n equations; l constraints reduce the effective number of independent components $k = n - l$.

2.3. Assembling of the governing system in holonomic and non-holonomic versions

Independence of virtual displacements with respect to constraints:

$$\nabla_{\mathbf{u}^{(q)}} \varphi^T(\mathbf{u}, \dots, \mathbf{u}^{(q)}, t) \delta \mathbf{u} = 0 \implies \mathbf{A} \cdot \delta \mathbf{u} = 0, \quad \mathbf{A} \in \mathbb{R}^{l,n} \quad \dots \dots \dots \quad l \text{ equations}$$

Sub-matrix: $\mathbf{A}^l \in \mathbb{R}^{l,l} : \det \mathbf{A}^l = \begin{vmatrix} a_{11}, a_{12}, \dots, a_{1l} \\ \vdots & \ddots & \vdots \\ a_{l1}, a_{2l}, \dots, a_{ll} \end{vmatrix} \neq 0, \quad \delta u_{l+1}, \dots, \delta u_n \quad \text{arbitrary variations}$

Variation of the extended functional:

$$\delta S\{\mathbf{u}\} = \int_0^{t_1} \left[(-1)^p \frac{d^p}{dt^p} (\nabla_{\mathbf{u}^{(p)}}^T \mathcal{T}(t)), \dots, -\frac{d}{dt} (\nabla_{\mathbf{u}^{(1)}}^T \mathcal{T}(t)) + \nabla_{\mathbf{u}}^T (\mathcal{T}(t) - \mathcal{V}(t)) + \nabla_{\mathbf{u}^{(q)}} \varphi^T \boldsymbol{\lambda}^T \right] \delta \mathbf{u} dt = 0.$$

Lagrangian equations of motion:

$$(-1)^p \frac{d^p}{dt^p} (\nabla_{\mathbf{u}^{(p)}}^T \mathcal{T}(t)), \dots, -\frac{d}{dt} (\nabla_{\mathbf{u}^{(1)}}^T \mathcal{T}(t)) + \nabla_{\mathbf{u}}^T (\mathcal{T}(t) - \mathbf{I}^T \mathcal{V}(t)) = \mathbf{Q} + \nabla_{\mathbf{u}^{(q)}} \varphi^T \boldsymbol{\lambda}^T \quad \dots n \text{ equations}$$

$\mathbf{u} = [u_1, \dots, u_n] \in \mathbb{R}^n$ - unknown components of the movement vector,
 $\boldsymbol{\lambda} = \boldsymbol{\lambda}(t) \in \mathbb{R}^l$ - l unknown Lagrange multipliers, $\boldsymbol{\lambda}(t)$ usually forces in reactions,
 $n + l$ equations together.

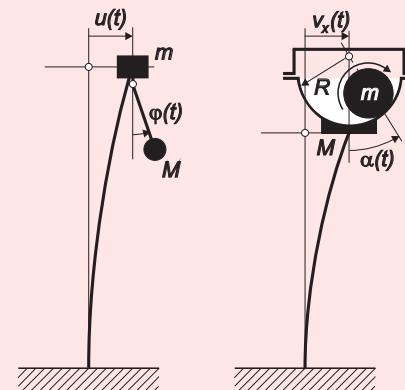
linear constraints - $\boldsymbol{\lambda}$ can be sometimes eliminated,
 n equations remain ($n - l$: movement, l : constraints).

3. DEMONSTRATION OF INDIVIDUAL SYSTEMS

3.1. First order linear constraints

Non-holonomic constraints (Pfaff type):

$$\begin{aligned}\dot{u}_{Cx} &= \omega_y(u_{Cz} - R) - \omega_z u_{Cy}, \\ \dot{u}_{Cy} &= \omega_z u_{Cx} - \omega_x(u_{Cz} - R), \\ \dot{u}_{Cz} &= \omega_x u_{Cy} - \omega_y u_{Cx},\end{aligned}$$

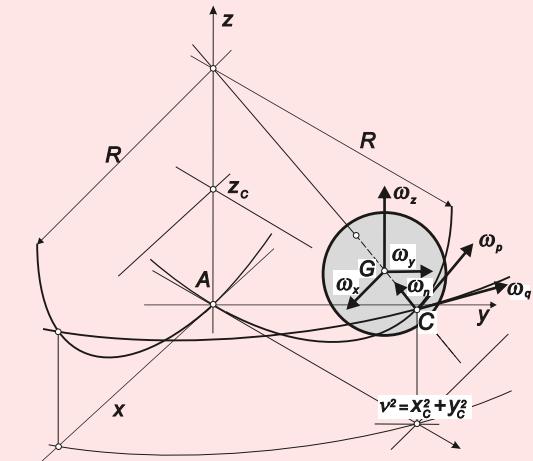


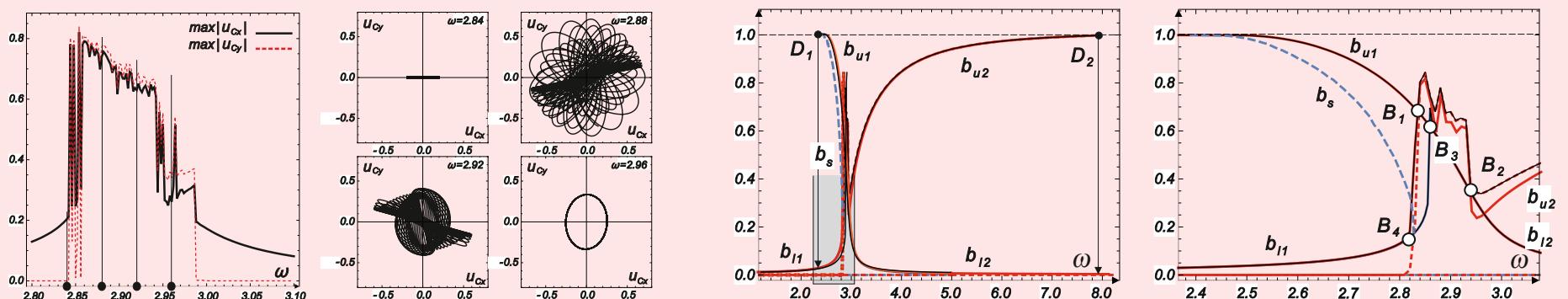
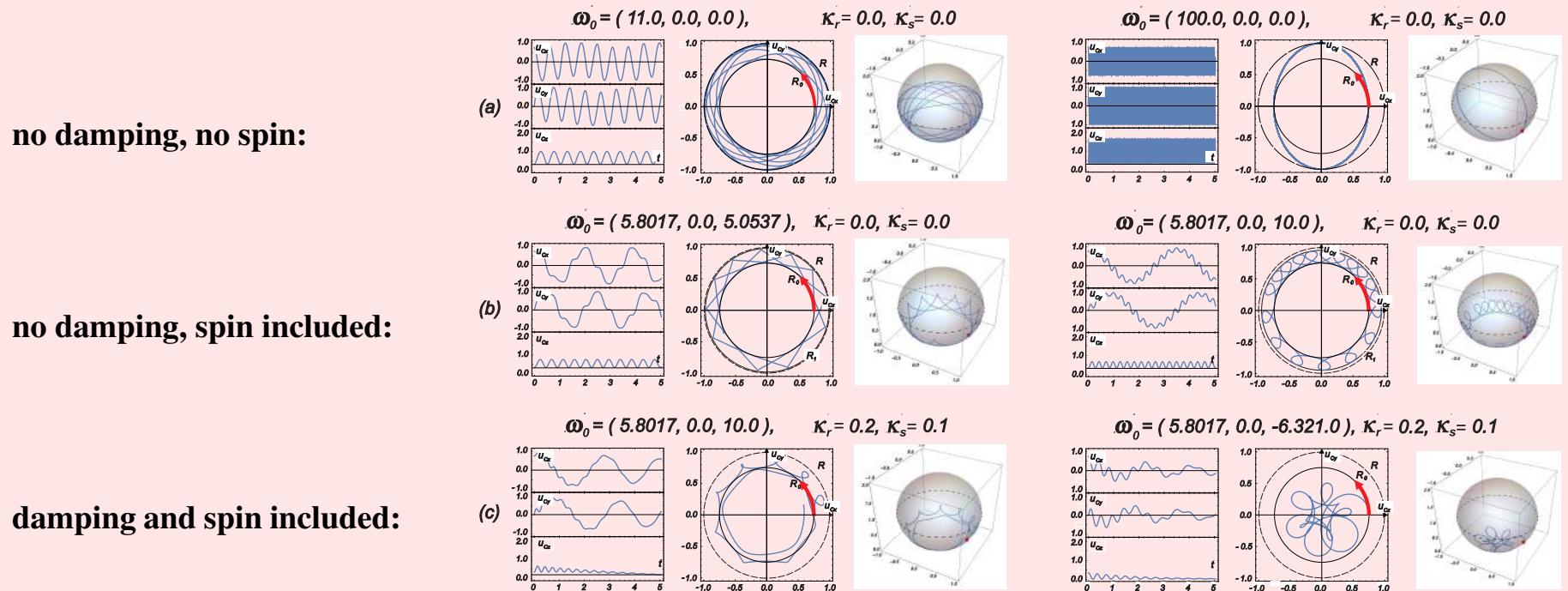
Equations of movement:

$$\begin{aligned}J_s \dot{\omega}_x &= ((\ddot{u}_{Ay} + \rho(\omega_z \dot{u}_{Cx} - \omega_x \dot{u}_{Cz})) (u_{Cz} - R) - \\ &\quad - u_{Cy} (g + \rho(\omega_x \dot{u}_{Cy} - \omega_y \dot{u}_{Cx}))) / \rho - D_{Gx}/M, \\ J_s \dot{\omega}_y &= (-(\ddot{u}_{Ax} + \rho(\omega_y \dot{u}_{Cz} - \omega_z \dot{u}_{Cy})) (u_{Cz} - R) + \\ &\quad + u_{Cx} (g + \rho(\omega_x \dot{u}_{Cy} - \omega_y \dot{u}_{Cx}))) / \rho - D_{Gy}/M, \\ J_s \dot{\omega}_z &= ((\ddot{u}_{Ax} + \rho(\omega_y \dot{u}_{Cz} - \omega_z \dot{u}_{Cy})) u_{Cy} - \\ &\quad - (\ddot{u}_{Ay} + \rho(\omega_z \dot{u}_{Cx} - \omega_x \dot{u}_{Cz})) u_{Cx}) / \rho - D_{Gz}/M.\end{aligned}$$

$$J_s = \underbrace{(J + M\rho^2 R^2)} / M\rho^2,$$

mass inertia moment of the ball



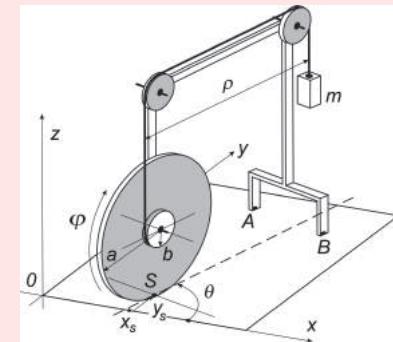


3.2. First order nonlinear constraints

Basic relations:

$$u_x = u_{xs} + \rho \cos \theta, \quad u_y = u_{ys} + \rho \sin \theta, \quad du_z = b d\varphi$$

Appell-Hamel dynamic system.



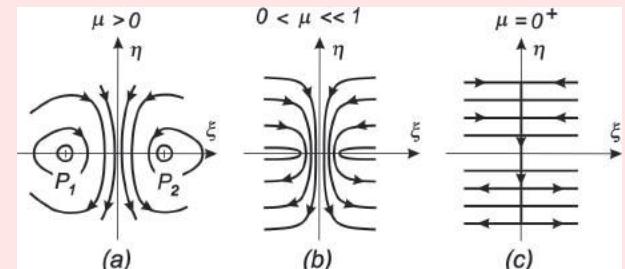
Non-holonomic (Pfaff) constraints:

$$\dot{u}_{xs} = a\dot{\varphi} \cos \theta, \quad \dot{u}_{ys} = a\dot{\varphi} \sin \theta$$

Kinetic and potential energies:

$$\begin{aligned}\mathcal{T}(t) &= \frac{1}{2}m(\dot{u}_x^2 + \dot{u}_y^2 + \dot{u}_z^2) + \frac{1}{2}M(\dot{u}_{xs}^2 + \dot{u}_{ys}^2) + \frac{1}{2}(J_z\dot{\theta}^2 + J_c\dot{\varphi}^2), \\ \mathcal{V}(t) &= mg(H_0 - u_z)\end{aligned}$$

Trajectories of the contact point - $\mu \geq 0$



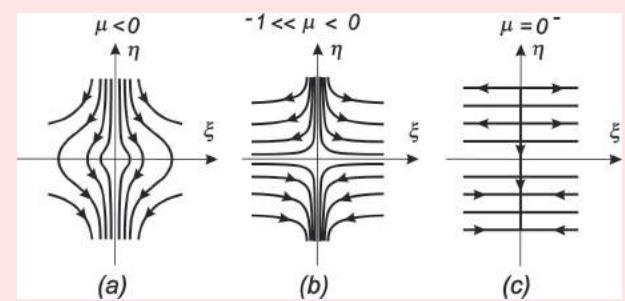
Lagrange equations:

$$\begin{aligned}(J_z + m\rho^2)\ddot{\theta} + m a \rho \cdot \theta \ddot{\varphi} &= 0, \\ ((m + M)a^2 + mb^2 + J_c)\ddot{\varphi} + m a \rho \cdot \dot{\theta}^2 + mg b &= 0.\end{aligned}$$

Reduced form ($M = J_z = J_c = 0$) \implies :

$$\rho \ddot{\theta} + a \dot{\theta} \dot{\varphi} = 0, \quad (a^2 + b^2) \ddot{\varphi} - a \rho \dot{\theta}^2 = -gb.$$

Trajectories of the contact point - $\mu \leq 0$



movement: $\dot{u}_x \ddot{u}_y - \ddot{u}_x \dot{u}_y = 0, \quad (a^2 + b^2) \ddot{u}_z = -gb^2,$

constraint: $\dot{u}_x^2 + \dot{u}_y^2 = \frac{a^2}{b^2} \dot{u}_z^2.$

3.3. Second order linear constraints

Non-holonomic constraint specifying pseudo-precession:

$$(\omega_\xi \dot{\omega}_\eta - \dot{\omega}_\xi \omega_\eta) + \omega_\zeta (\omega_\xi^2 + \omega_\eta^2) - \lambda (\omega_\xi^2 + \omega_\eta^2)^{3/2} = 0$$

$$(\ddot{\psi}\dot{\theta} - \dot{\theta}\ddot{\psi}) \sin \theta + (2\dot{\psi}\dot{\theta}^2 + \dot{\psi}^3 \sin^2 \theta) \cos \theta + \lambda (\dot{\varphi}^2 + \dot{\theta}^2)^{3/2} = 0$$

Euler angles:

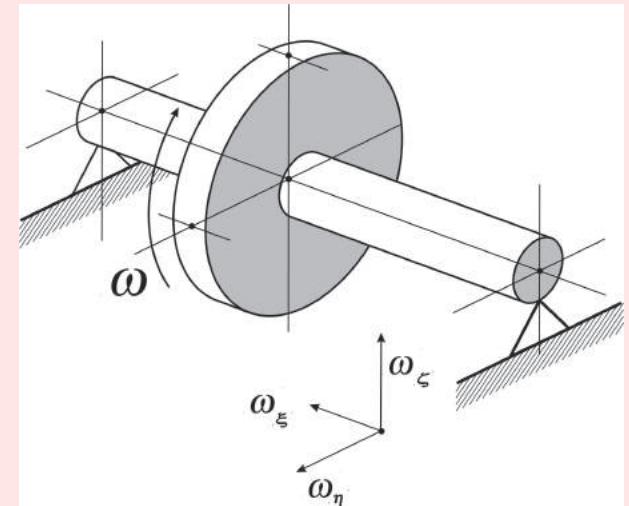
$$\omega_\xi = \dot{\psi} \sin \theta \sin \varphi + \dot{\theta} \cos \varphi,$$

$$\omega_\eta = \dot{\psi} \sin \theta \cos \varphi - \dot{\theta} \sin \varphi,$$

$$\omega_\zeta = \dot{\psi} \cos \theta + \dot{\varphi}$$

When $\dot{\varphi}, \dot{\psi}$ are constants and $\dot{\theta}$ vanishes, the regular precession emerges. Non-trivial variable $\dot{\varphi}, \dot{\psi}, \dot{\theta}$ lead to precession. Then it is necessary to investigate the rate of stability of the precession phenomenon.

Rotating shaft - pseudo-precession.



3.4. Third order linear constraints

Lagrange function:

$$\mathcal{T} = \frac{1}{2}m(\dot{u}_x^2 + \dot{u}_y^2) + \lambda L$$

Lagrange equations:

$$m\ddot{u}_x = Q_x + \lambda L u_x, \quad m\ddot{u}_y = Q_y + \lambda L u_y,$$

Q_x, Q_y - external forces acting along axes x, y .

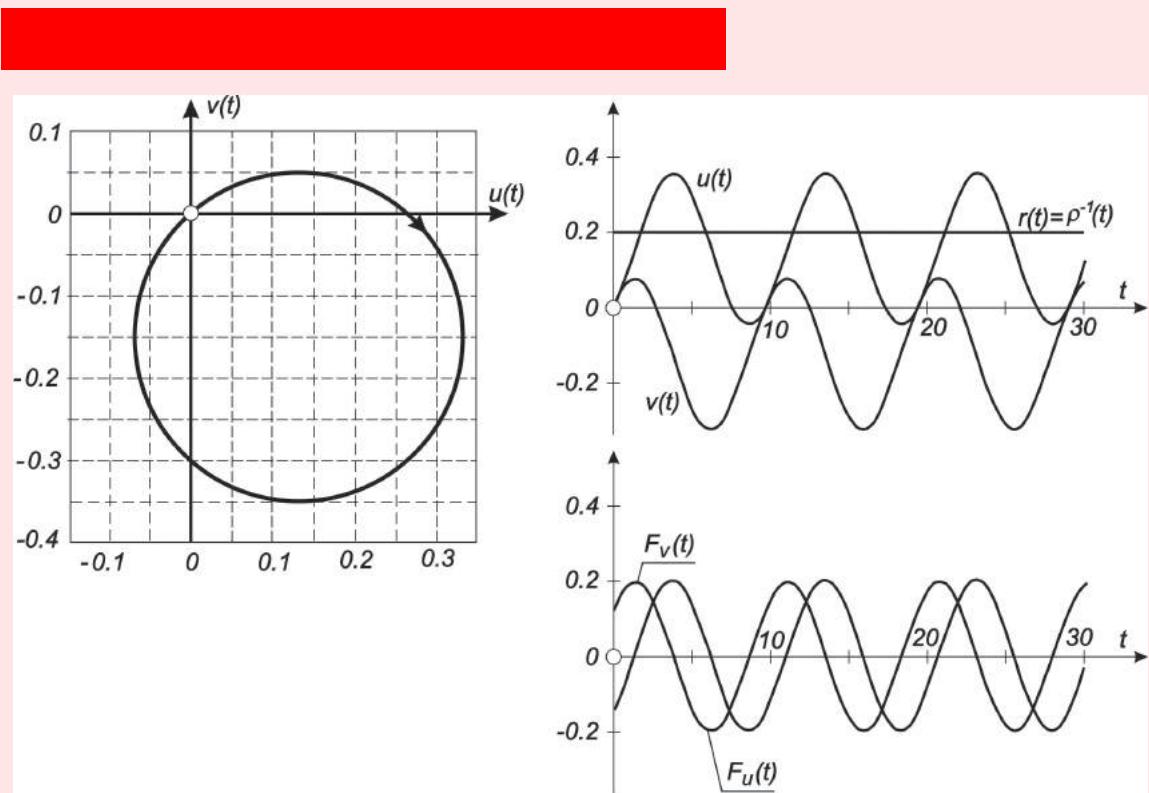
Curvature - planar trajectory:

$$\varrho(t) = \frac{\dot{u}_x \ddot{u}_y - \ddot{u}_x \dot{u}_y}{(\dot{u}_x^2 + \dot{u}_y^2)^{3/2}}$$

Curvature time derivative:

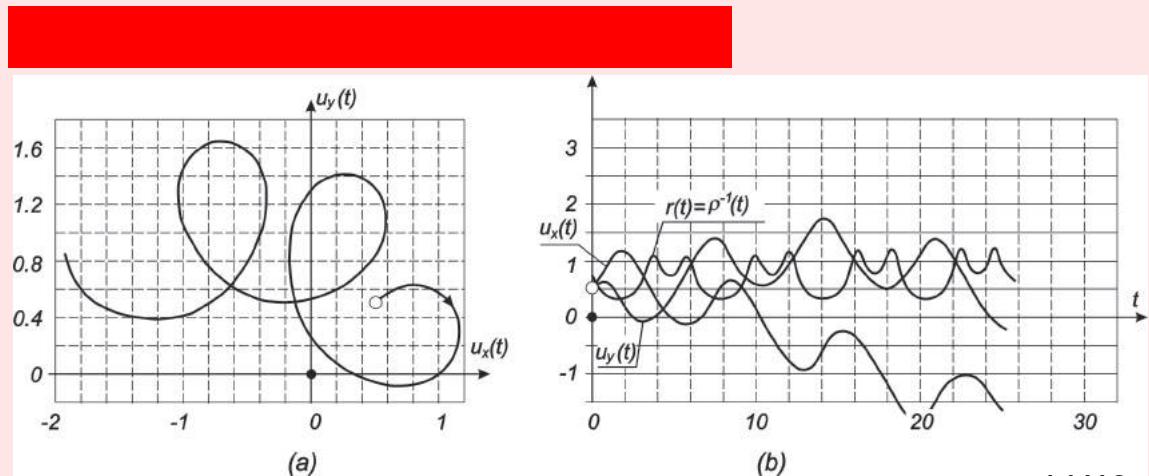
$$\dot{\varrho}(t) = \frac{\dot{u}_x \ddot{u}_y - \ddot{u}_x \dot{u}_y}{(\dot{u}_x^2 + \dot{u}_y^2)^{3/2}} - 3\varrho(t) \frac{\dot{u}_x \ddot{u}_x + \dot{u}_y \ddot{u}_y}{\dot{u}_x^2 + \dot{u}_y^2}$$

$\dot{\varrho}(t), \varrho(t)$ - prescribed functions of time.



$$m(\ddot{u}_x \dot{u}_x + \ddot{u}_y \dot{u}_y) = Q_x \dot{u}_x + Q_y \dot{u}_y,$$

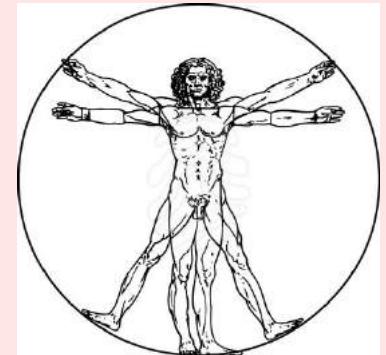
$$(\dot{u}_x \ddot{u}_y - \ddot{u}_x \dot{u}_y)(\dot{u}_x \ddot{u}_y - \ddot{u}_x \dot{u}_y) = -\varrho^2 (\dot{u}_x^2 + \dot{u}_y^2)^3 + 3\varrho \dot{\varrho} (\dot{u}_x \ddot{u}_x + \dot{u}_y \ddot{u}_y).$$



4. CONCLUSION - CREED OF RATIONAL MECHANICS

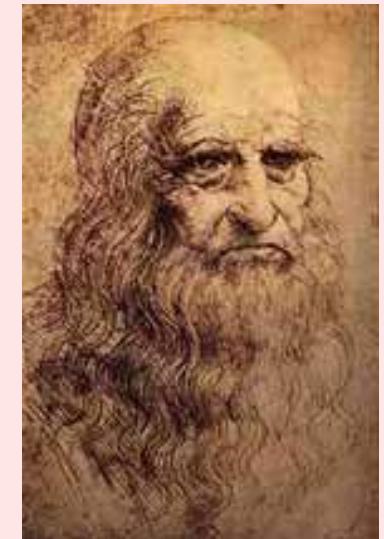
- La meccanica e il paradiso delle scienze matematiche,
perché con quella si viene al frutto matematico.

*Mechanics is the paradise of the mathematical sciences,
because with it we come to the most beautiful fruits of mathematical knowledge.*



- Si come il mangiare senza voglia fia dannoso alla salute,
così lo studio senza desiderio guasta la memoria, e no' ritiene cosa ch'ella pigli.

*Like eating tasteless is harmful to health,
so study without desire spoils the memory, and it cannot keep you take.*



Leonardo da Vinci (1452 - 1519)

*** **Thank you for your patience** ***